



**CHEG 3128**

**Battery – 1**  
**Electrochemical Fundamentals**

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*Department of Chemical, Materials and Biomolecular Engineering*

# Redox Processes

- Reduction

- Electron Accepting



- Oxidation

- Electron Donating

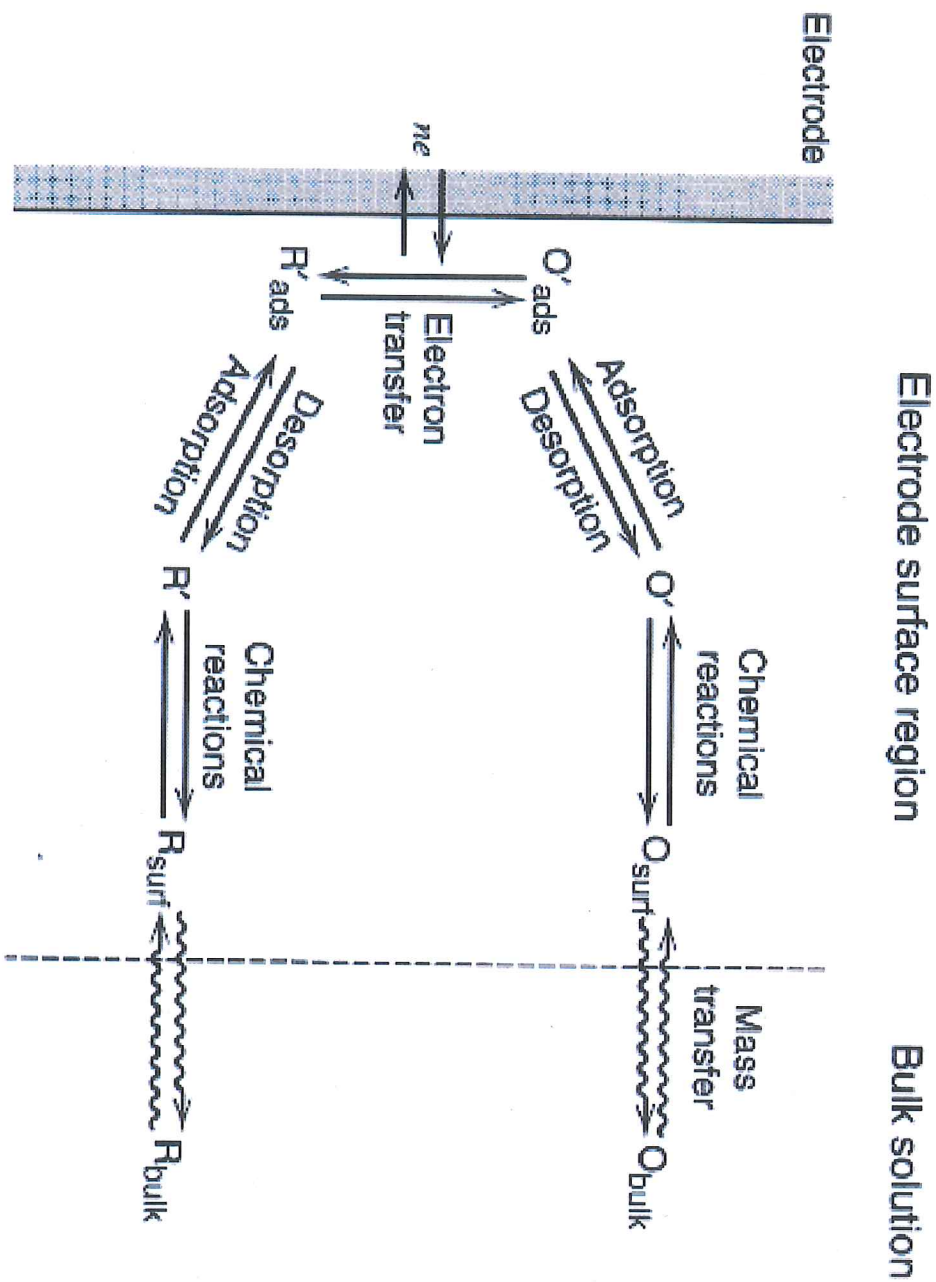


- Equilibrium



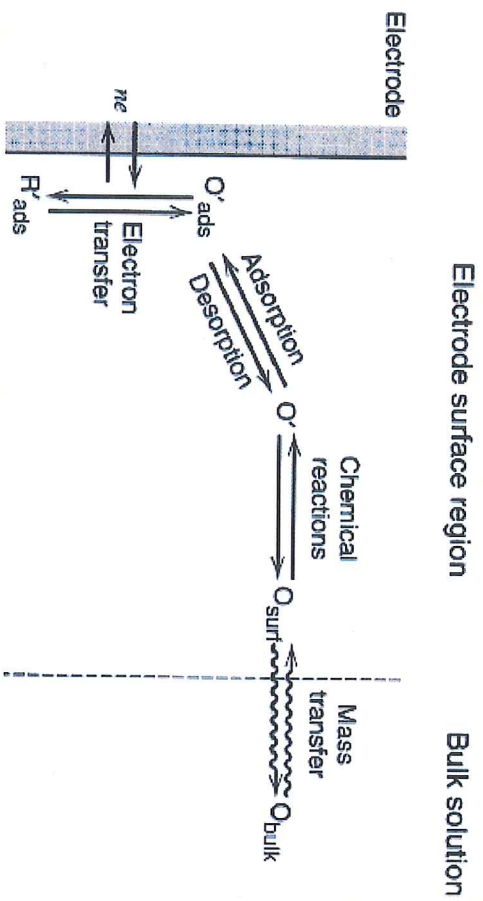
- Always written in the reduction form

# All Electrochemical Processes Occur on a surface



# Types of Reactions

## 1. Electrodeposition (reduction)

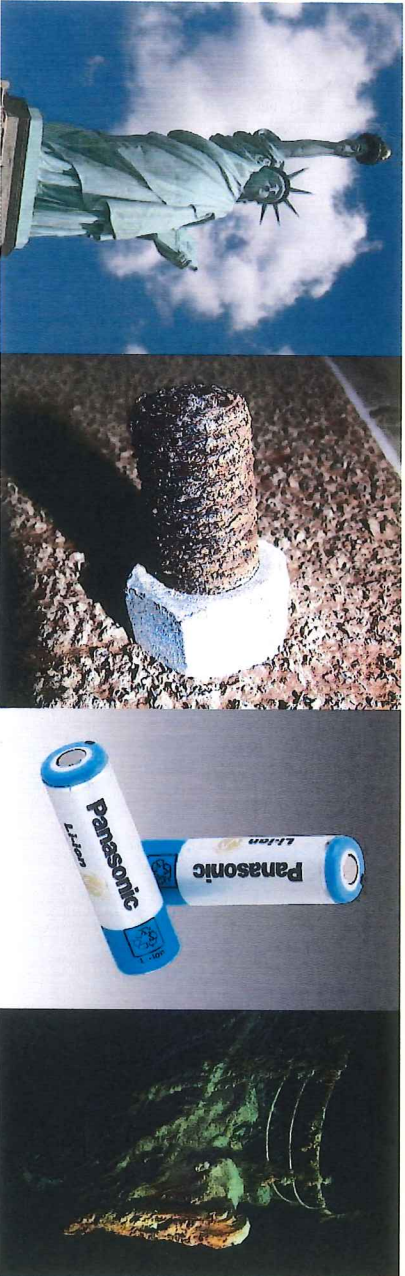
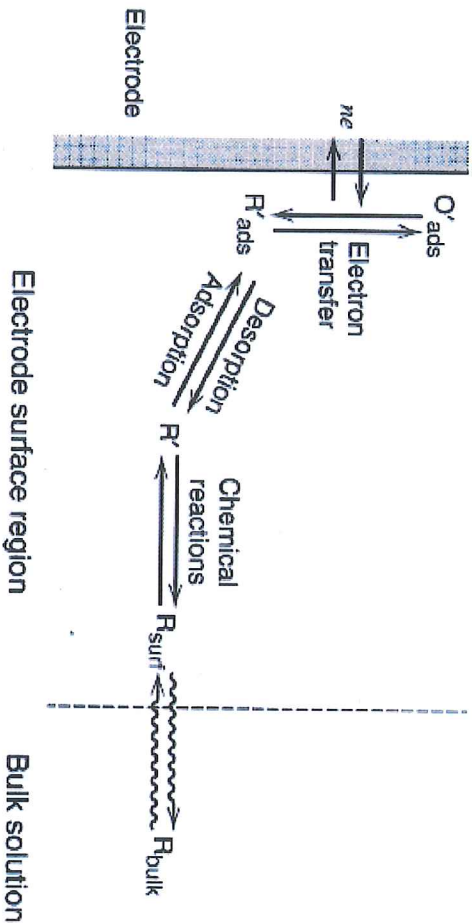


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# Types of Reactions

## 2. Corrosion (oxidation)

- $\text{Fe(s)} \rightarrow \text{Fe}^{+3} + 3\text{e}^-$
- $\text{Li(s)} \rightarrow \text{Li}^+ + \text{e}^-$
- $\text{Cu(s)} \rightarrow \text{Cu}^{+2} + 2\text{e}^-$



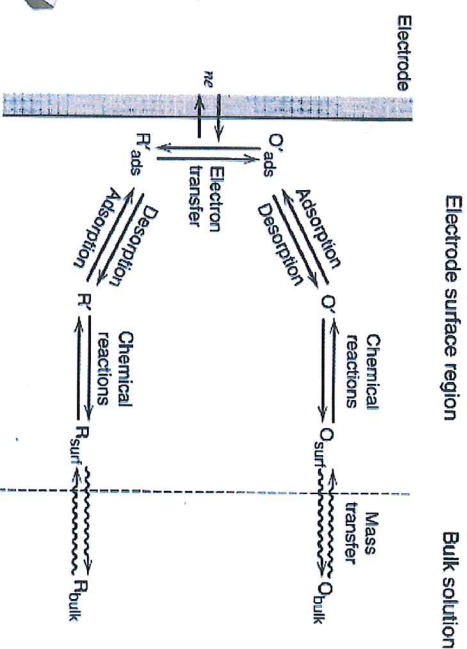
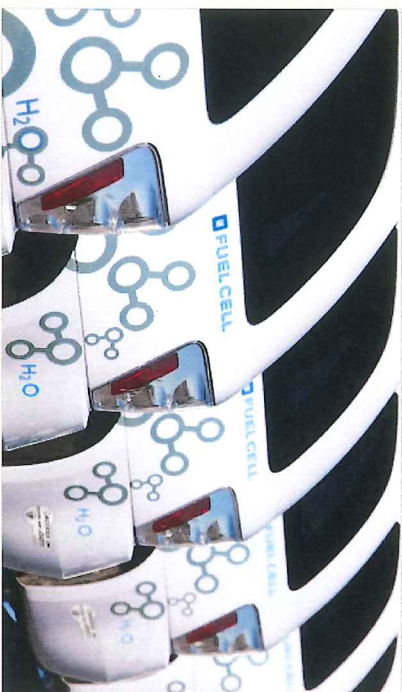
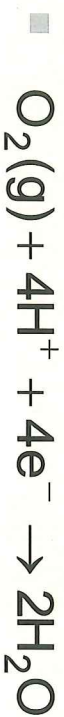
# Types of Reactions

## 3. Electrocatalysis

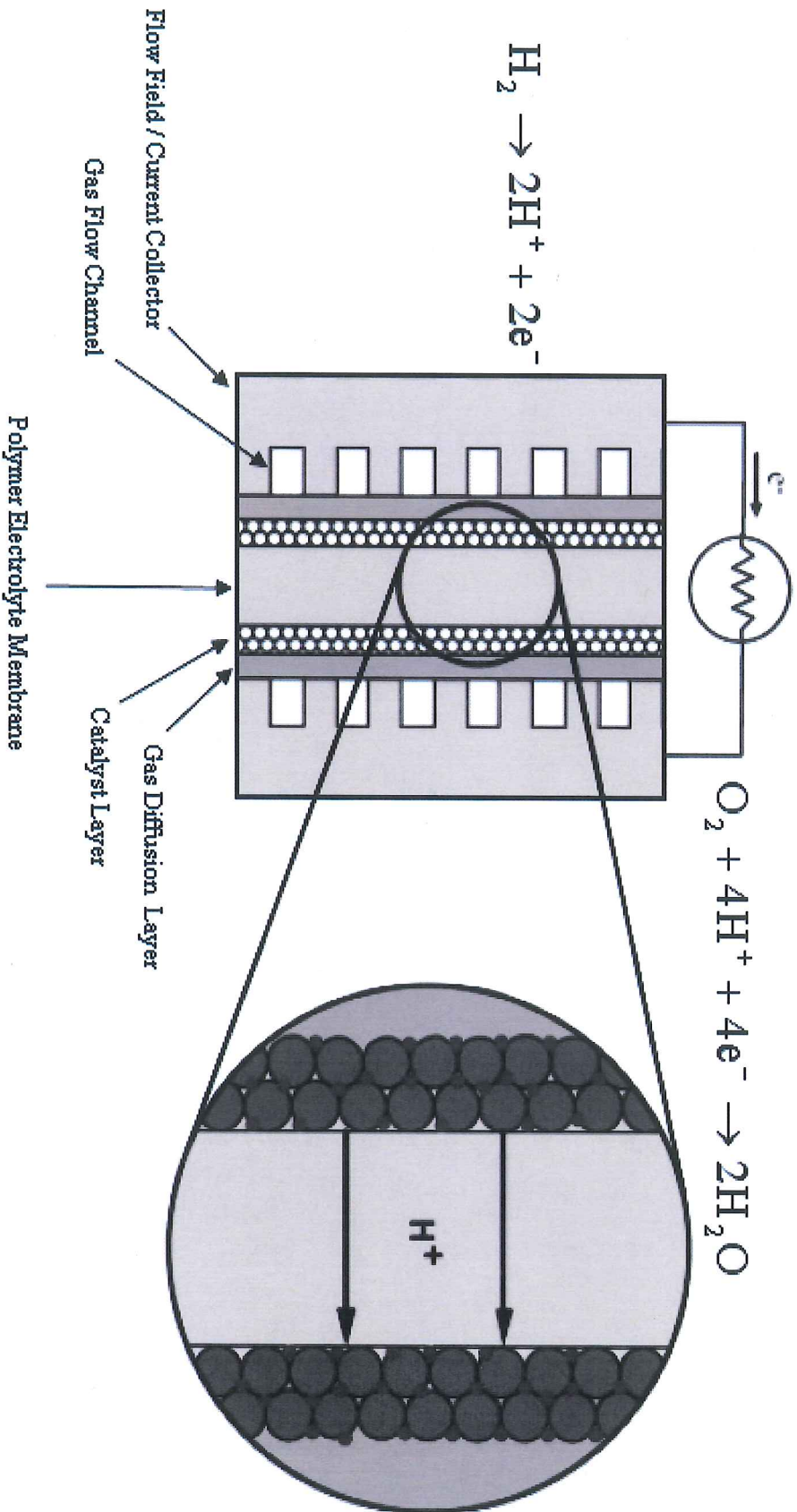
### i) Pure Redox



### ii) Traditional Catalysis



# Example Cell : Proton Exchange Membrane Fuel Cell



# Anode and Cathode

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- Faradaic and non-faradaic processes
  - Faradaic – electrochemical reactions
    - Note: Electrochemical reactions have both chemical and electrochemical steps! What are the implications?
  - Non-faradaic – adsorption/desorption, double layer charging/discharging (we'll discuss this in detail next time)
- Must be electrically conducting
- Minimize distance between them
  - Ionic movement through electrolyte is akin to a pure Ohmic resistance



# Electrolyte

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- Liquids: Dissolved salts in a solvent
    - Mostly discuss aqueous in this class
  - Solids: Ion conducting groups
  - Provides a media for ion transport
  - Since the electrolyte solvates the ions (which complete the electrochemical circuit), the reactant must also be solvated in the electrolyte to react
- 
- This leads to the so-called electrochemical “Three Phase Boundary”

# Three Phase boundary

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- For an electrochemical reaction to occur, we **MUST** have three things present
  - Reactant
  - Catalyst/Electrode
  - Electrolyte
- Designing this interface is critical for device performance
  - Void Space
    - Reactant mass transport
  - Maximize interface between catalyst and electrolyte



# NIST Chemistry Webbook

The screenshot shows a web browser window with the URL [webbook.nist.gov/chemistry/](http://webbook.nist.gov/chemistry/). The page title is "NIST Chemistry WebBook" and the main heading is "NIST Standard Reference Database Number 69". Below the heading, there is a "View:" section with a link to "Search Options, Models and Tools, Special Data Collections, Documentation, Changes, Note". A "Credits" link is also present. A "Search Options" section is expanded, showing two categories: "General Searches" and "Physical Property Based Searches". The "General Searches" category includes links for Formula, Name, IUPAC identifier, CAS registry number, Reaction, Author, and Structure. The "Physical Property Based Searches" category includes links for Ion energetics properties, Vibrational and electronic energies, and Molecular weight. Below the search options, there is a "Models and Tools" section with a list of links: "Thermophysical Properties of Fluid Systems: High accuracy data for a select group of fluids.", "Group Additivity Based Estimates: Estimates of gas phase thermodynamic properties based on a submitted structure.", and "Formula Browser: Locates chemical species by building up a chemical formula in Hill order." The browser's taskbar at the bottom shows various application icons and the system clock indicating 1:30 PM on 1/9/2017.

Microsoft Office Home X Calendar - Musain, Will X Mail - Musain, William X Hozier - Take Me To 41 X NIST Chemistry WebBook X

Apps Office 365 ESPN: The Worldwid: Yahoo - Email login Netflix

## NIST Chemistry WebBook

### NIST Standard Reference Database Number 69

View: [Search Options, Models and Tools](#), [Special Data Collections](#), [Documentation](#), [Changes](#), [Note](#)

[Credits](#)

NIST reserves the right to change for access to this database in the future.

#### Search Options top

General Searches	Physical Property Based Searches
<ul style="list-style-type: none"><li>• Formula</li><li>• Name</li><li>• IUPAC identifier</li><li>• CAS registry number</li><li>• Reaction</li><li>• Author</li><li>• Structure</li></ul>	<ul style="list-style-type: none"><li>• Ion energetics properties</li><li>• Vibrational and electronic energies</li><li>• Molecular weight</li></ul>

#### Models and Tools top

- [Thermophysical Properties of Fluid Systems: High accuracy data for a select group of fluids.](#)
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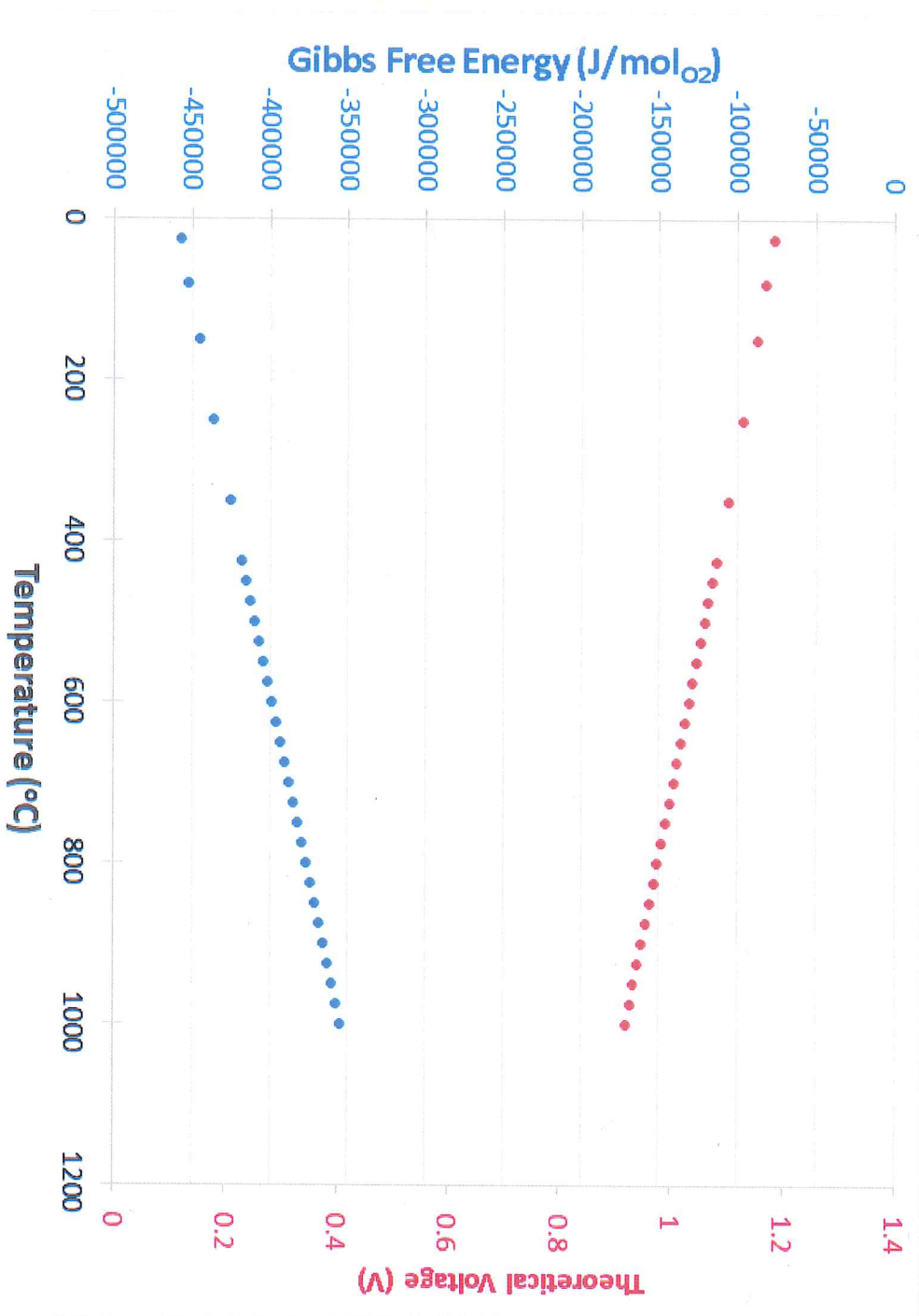
# Chemical Engineering Junior Lab (CHEG 3128)

## Spring 2017

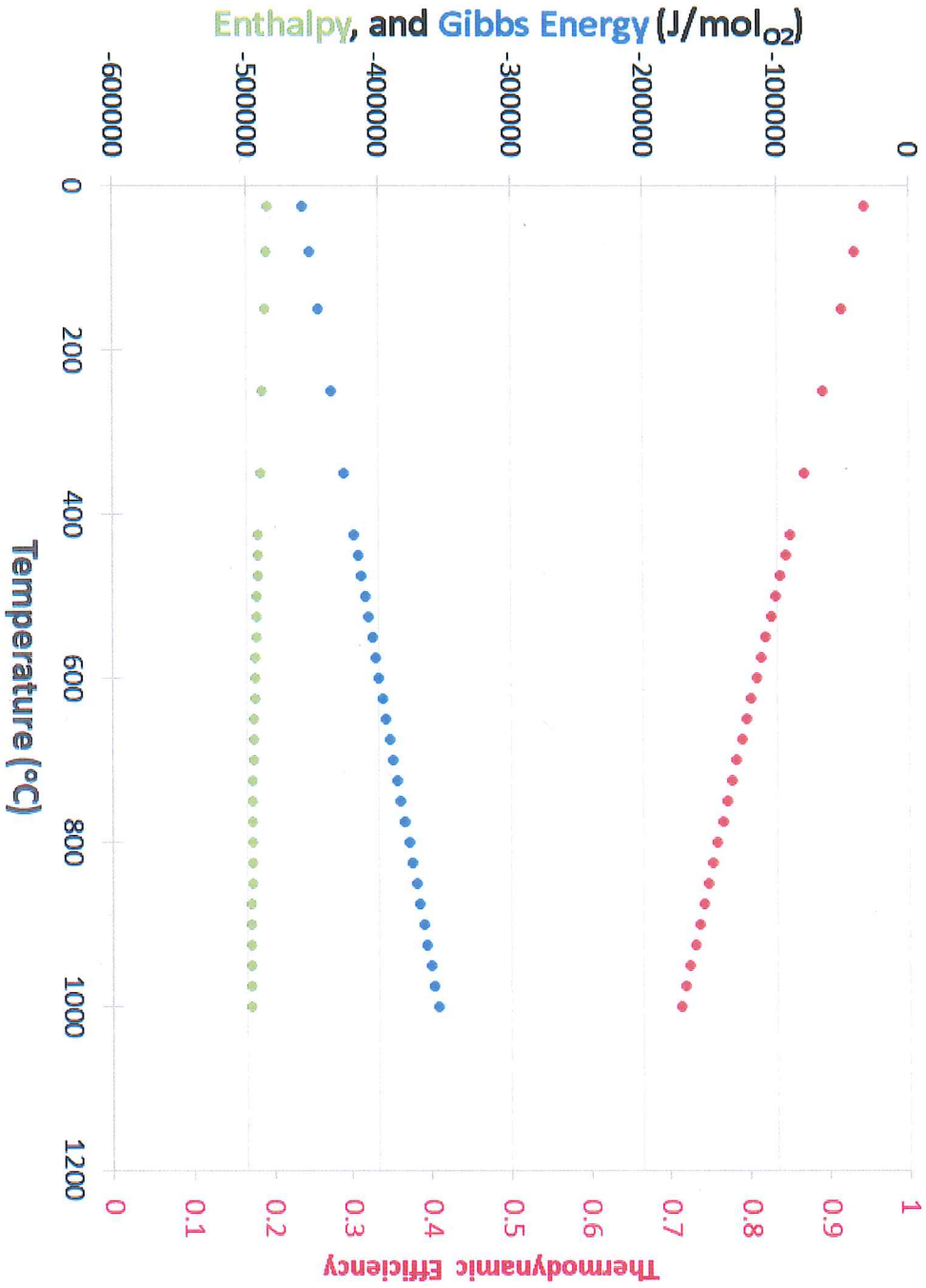
# ΔG (T) for $2H_2 + O_2 \rightarrow 2H_2O$

Species	Hof (kJ/mol)	S <sub>0</sub> (J/mol <sup>o</sup> K)	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	AA	AB	AC	AD	AE	AF	AG	AH	AI	AJ	AK	AL	AM	AN	AO	AP	AQ	AR	AS	AT	AU	AV	AW	AX	AY	AZ					
Methane	-74.87	186.25	-0.20929	108.479	-42.5317	5.80738	0.67865	-76.4936	18.7165	-74.8731	186.2501	205.1472	393.5234	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0						
CO <sub>2</sub>	-393.52	213.79	-0.23975	55.18966	-18.6017	7.96387	-0.00728	-403.0975	228.2441	-393.5234	213.7901	319.4746	675.9106	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0				
Hydrogen	0	205.15	31.32334	-11.26341	13.49316	-2.77374	-0.13858	-9.98977	12.70794	0	205.1472	319.4746	675.9106	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Carbon	716.669	158.1	21.792	-0.81248	0.44857	-0.04326	0.00219	710.347	183.8724	716.669	158.1001	266.7131	509.9371	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
H <sub>2</sub> O	-110.33	188.84	30.992	6.82514	6.79435	-2.53448	0.00219	-250.881	223.3667	-110.3274	188.8401	266.7131	509.9371	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
CO	-130.53	197.66	25.50799	6.68813	4.65466	-2.67188	0.131021	-118.0089	227.3665	-130.5274	197.6601	266.7131	509.9371	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	

$C = A + B + C + D + E + F + G$   
 $H = H_f + \int_{T_0}^T \frac{C_p}{T^2} dT + \frac{C}{T} - \frac{C_0}{T_0}$   
 $S = S_0 + \int_{T_0}^T \frac{C_p}{T} dT + R \ln \frac{P}{P_0}$   
 $\Delta G = \Delta H - T \Delta S$



# $\Delta H (T)$ and $\Delta G (T)$ for $2H_2 + O_2 \rightarrow 2H_2O$



# Extra Resources

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- “Electrochemical Methods: Fundamentals and Applications”, 2<sup>nd</sup> Edition. Allen J. Bard and Larry R. Faulkner.

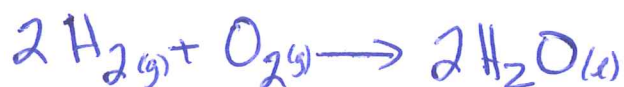


# CHEG 3128 - Battery 1

All reactions are electron transfer processes

- what I mean is that every reacting system is a combination of complementary redox reactions.

For instance, take the combustion of  $H_2$



→ Is this spontaneous? Exo/Endo thermic?

→ How do we capture energy?

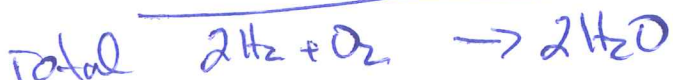
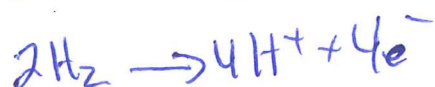
→ As heat →  $\Delta H(t)$

→ In this reaction, what is oxidized?

"

, what is reduced?

What if I write it like this:



Reductions are  $e^-$  accepting reactions

Oxidations are  $e^-$  donation reactions

∴ H is oxidized from  $H(0) \rightarrow H(+)$

O is reduced from  $O(0) \rightarrow O(2-)$

In a chemical system, we recover the energy from this RXN as heat.  $H_2$  combustion is used in combined cycle power plants. The combustion heat creates steam, which turns a turbine, spinning a shaft between 2 magnets & looped Cu wire  $\rightarrow$  the rotation of the shaft in the magnetic field (Physics 2!) produces a current.

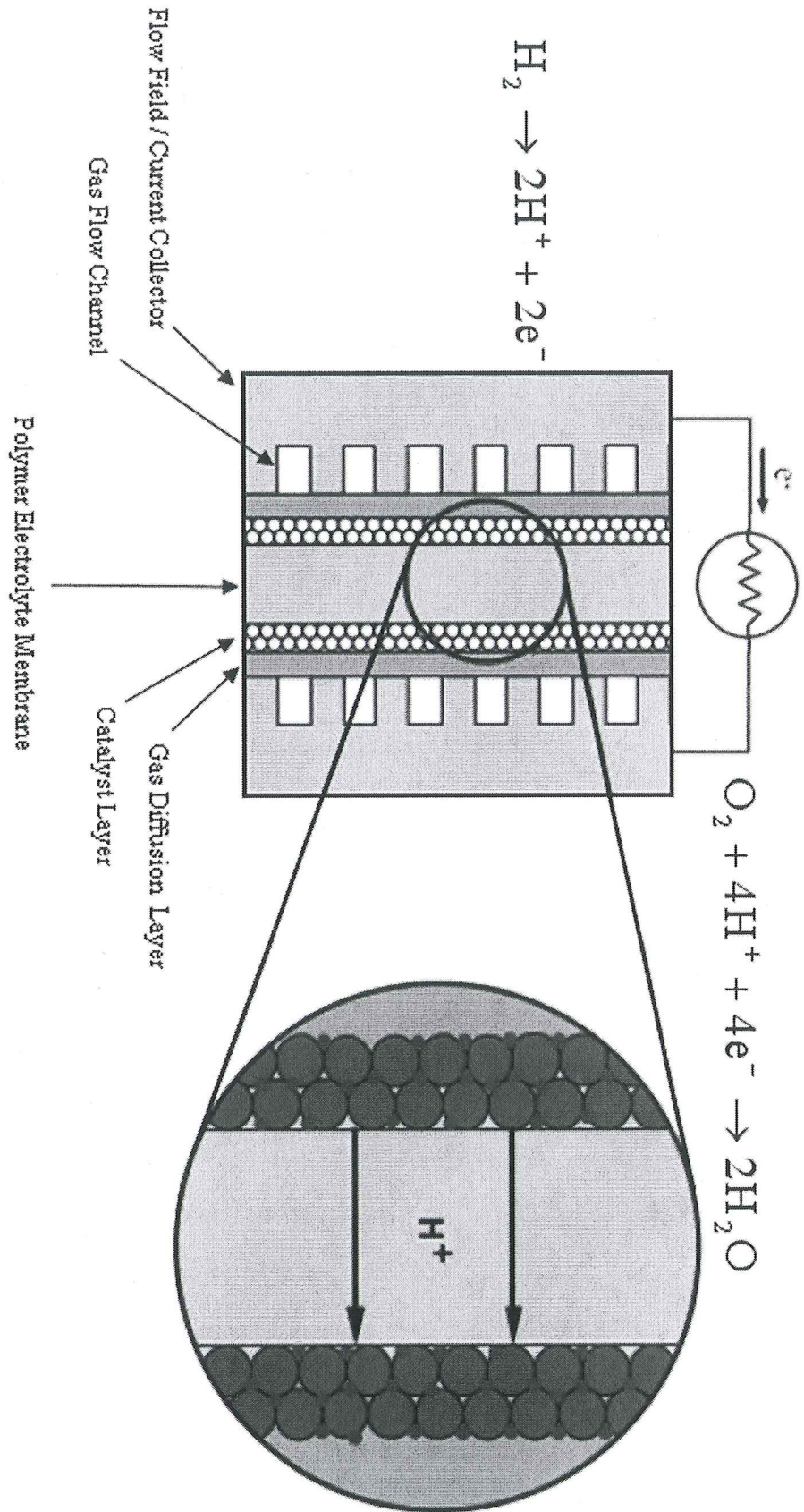
What if we didn't need to do that? What if we could directly use the electrons from the  $1/2$  reactions?  $\rightarrow$  this is electrochemical engineering. One such system is a proton exchange membrane fuel cell.

$\hookrightarrow$  Diagram on next page

$\rightarrow$  oxidations happen @ the anode  
- (-) "negative" electrode

$\rightarrow$  reduction happen @ the cathode  
- (+) "positive" electrode

How much energy can we get from electrochemical processes?



Let's do an energy / Entropy Balance on one electrode:



Generalized Energy Balance

$$U_E = U_B + \sum H_{in}^{mass} - \sum H_{out}^{mass} + Q + W$$

- Break up work term:

$$W = - (P\Delta V + W_{elec})$$

$$U_E = U_B + \sum H_{in}^{mass} - \sum H_{out}^{mass} + Q - P\Delta V - W_{elec}$$

Assumptions: 1) Closed System

2) All electrochemical RXNs are reversible

$$U_E = U_B + Q - P\Delta V - W_{ELEC}$$

$$S_E = S_B + \frac{Q}{T}$$

$$Q = T\Delta S$$

$$U_E - U_B + P\Delta V = Q - W_{ELEC}$$

$$\Delta U + P\Delta V = T\Delta S - W_{ELEC}$$

$$\Delta H - T\Delta S = -W_{elec}$$

$$\Delta G = -W_{elec}$$

$$\boxed{W_{elec} = -\Delta G}$$

Units:  $W = \frac{J}{mol} = \frac{E \cdot C}{mol} = \text{change} \cdot \text{potential}$   
 $= Q \cdot E$

$$Q = \frac{\text{charge}}{\text{mole reactant}} = n \cdot F$$

$$\frac{\text{mole } e^-}{\text{mol reactant}} \cdot \frac{C}{\text{mole } e^-}$$

$$W = -\Delta G = nFE$$

$$\boxed{\Delta G = -nFE}$$



@ STP, 25°C, 1 bar (or 1M)

$$\Delta G^\circ = -nFE^\circ$$

where  $E^\circ$  is called the "Standard Potential"

How to find the standard potential for an individual reaction?

First, know that we ~~cannot~~ it impossible to know how much energy ~~we~~ have in a system, which is why we ALWAYS report them as  $\Delta G$ ,  $\Delta H$ , etc.

Therefore, we need an internal standard



$$E_{\text{H}^+/\text{H}_2}^\circ = 0.0\text{V}$$

# Oxygen Reduction in acid media



$$\Delta g_{f, \text{H}_2\text{O}}^\circ = -237,200 \text{ J/mol}$$

$$\Delta g_{f, \text{O}_2}^\circ = 0 \text{ J/mol}$$

$$\Delta g_{f, \text{H}_2}^\circ = 0 \text{ J/mol}$$

$$\Delta G^\circ = 2(-237,200 \text{ J/mol}) - [0 \text{ J/mol} + 2(0 \text{ J/mol})]$$

$$\Delta G^\circ = -474,400 \text{ J/mol}$$

$$\Delta G_{\text{rxn}}^\circ = -nFV_{\text{Th}}$$

$$V_{\text{Th}} = \frac{-\Delta G_{\text{rxn}}^\circ}{nF} = \frac{-(-474,400 \text{ J/mol})}{4 \text{ mol e}^-/\text{mol} \cdot 96485.3 \text{ C/mol e}^-} = 1.229 \text{ V}$$

you could also use this to determine specific potentials where reactions occur

$$V_{\text{Th}} = E_{\text{Cathode}}^\circ - E_{\text{Anode}}^\circ$$

↓  
Positive cell voltages mean spontaneous!  
↓  
galvanic cell

$$1.229 = E_{\text{Cathode}}^\circ - 0.0 \text{ V}$$

$$E_{\text{O}_2}^\circ = 1.229 \text{ V}$$

Do we need to do that work every time?

No → most electrochemical ~~couple~~ redox couples are tabulated

→ Some can be found in Appendix C

- Page 808 in B&E, Ed 2

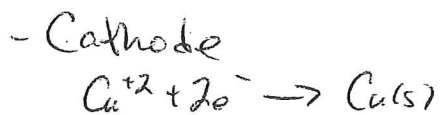
→ Also attached to next page

How does our ORR calculated  $E^\circ$  compare with the Table? They are EXACTLY THE SAME!

Now, let's answer our question about the Daniell cell....

What if we attached the - Cu foil to the  $\oplus$  terminal

- Cathode



- Zn foil to the  $\ominus$  terminal

- Anode



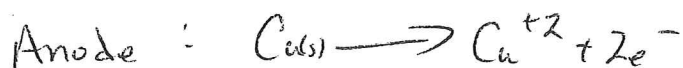
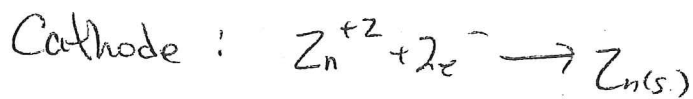
$$E_{\text{Cu}/\text{Cu}^{+2}}^{\circ} = 0.34 \text{ V}$$

$$E_{\text{Zn}/\text{Zn}^{+2}}^{\circ} = -0.76 \text{ V}$$

$$V_{\text{Th}} = E_{\text{c}}^{\circ} - E_{\text{A}}^{\circ} = 0.34 \text{ V} - (-0.76 \text{ V}) = 1.1 \text{ V}$$

↓  
galvanic! will occur spontaneously

What if we connected this the other way?



$$V_{\text{Th}} = E_{\text{c}}^{\circ} - E_{\text{A}}^{\circ} = -0.76 - 0.34 = -1.1 \text{ V}$$

↓  
nonspontaneous!  
↳ Electrolytic cell

How would we "recharge" this cell?

Make  $\Delta G < 0$ , so, we have to apply a voltage  $> 1.1 \text{ V}$  on the cell to make it go!

→ that's why you plug your phone in!



APPENDIX

C

REFERENCE TABLES

TABLE C.1 Selected Standard Electrode Potentials in Aqueous Solutions at 25°C in V vs. NHE<sup>a</sup>

Reaction	Potential, V
$\text{Ag}^+ + e \rightleftharpoons \text{Ag}$	0.7991
$\text{AgBr} + e \rightleftharpoons \text{Ag} + \text{Br}^-$	0.0711
$\text{AgCl} + e \rightleftharpoons \text{Ag} + \text{Cl}^-$	0.2223
$\text{AgI} + e \rightleftharpoons \text{Ag} + \text{I}^-$	-0.1522
$\text{Ag}_2\text{O} + \text{H}_2\text{O} + 2e \rightleftharpoons 2\text{Ag} + 2\text{OH}^-$	0.342
$\text{Al}^{3+} + 3e \rightleftharpoons \text{Al}$	-1.676
$\text{Au}^+ + e \rightleftharpoons \text{Au}$	1.83
$\text{Au}^{3+} + 2e \rightleftharpoons \text{Au}^+$	1.36
$p\text{-benzoquinone} + 2\text{H}^+ + 2e \rightleftharpoons \text{hydroquinone}$	0.6992
$\text{Br}_2(\text{aq}) + 2e \rightleftharpoons 2\text{Br}^-$	1.0874
$\text{Ca}^{2+} + 2e \rightleftharpoons \text{Ca}$	-2.84
$\text{Cd}^{2+} + 2e \rightleftharpoons \text{Cd}$	-0.4025
$\text{Cd}^{2+} + 2e \rightleftharpoons \text{Cd}(\text{Hg})$	-0.3515
$\text{Ce}^{4+} + e \rightleftharpoons \text{Ce}^{3+}$	1.72
$\text{Cl}_2(\text{g}) + 2e \rightleftharpoons 2\text{Cl}^-$	1.3583
$\text{HClO} + \text{H}^+ + e \rightleftharpoons \frac{1}{2}\text{Cl}_2 + \text{H}_2\text{O}$	1.630
$\text{Co}^{2+} + 2e \rightleftharpoons \text{Co}$	-0.277
$\text{Co}^{3+} + e \rightleftharpoons \text{Co}^{2+}$	1.92
$\text{Cr}^{2+} + 2e \rightleftharpoons \text{Cr}$	-0.90
$\text{Cr}^{3+} + e \rightleftharpoons \text{Cr}^{2+}$	-0.424
$\text{Cr}_2\text{O}_7^{2-} + 14\text{H}^+ + 6e \rightleftharpoons 2\text{Cr}^{3+} + 7\text{H}_2\text{O}$	1.36
$\text{Cu}^+ + e \rightleftharpoons \text{Cu}$	0.520
$\text{Cu}^{2+} + 2\text{CN}^- + e \rightleftharpoons \text{Cu}(\text{CN})_2^-$	1.12
$\text{Cu}^{2+} + e \rightleftharpoons \text{Cu}^+$	0.159
$\text{Cu}^{2+} + 2e \rightleftharpoons \text{Cu}$	0.340
$\text{Cu}^{2+} + 2e \rightleftharpoons \text{Cu}(\text{Hg})$	0.345
$\text{Eu}^{3+} + e \rightleftharpoons \text{Eu}^{2+}$	-0.35
$1/2\text{F}_2 + \text{H}^+ + e \rightleftharpoons \text{HF}$	3.053
$\text{Fe}^{2+} + 2e \rightleftharpoons \text{Fe}$	-0.44
$\text{Fe}^{3+} + e \rightleftharpoons \text{Fe}^{2+}$	0.771
$\text{Fe}(\text{CN})_6^{3-} + e \rightleftharpoons \text{Fe}(\text{CN})_6^{4-}$	0.3610

(continued)

TABLE C.1 (continued)

Reaction	Potential, V
$2\text{H}^+ + 2e \rightleftharpoons \text{H}_2$	0.0000
$2\text{H}_2\text{O} + 2e \rightleftharpoons \text{H}_2 + 2\text{OH}^-$	-0.828
$\text{H}_2\text{O}_2 + 2\text{H}^+ + 2e \rightleftharpoons 2\text{H}_2\text{O}$	1.763
$2\text{Hg}^{2+} + 2e \rightleftharpoons \text{Hg}_2^{2+}$	0.9110
$\text{Hg}_2^{2+} + 2e \rightleftharpoons 2\text{Hg}$	0.7960
$\text{Hg}_2\text{Cl}_2 + 2e \rightleftharpoons 2\text{Hg} + 2\text{Cl}^-$	0.26816
$\text{Hg}_2\text{Cl}_2 + 2e \rightleftharpoons 2\text{Hg} + 2\text{Cl}^-$ (sat'd. KCl)	0.2415
$\text{HgO} + \text{H}_2\text{O} + 2e \rightleftharpoons \text{Hg} + 2\text{OH}^-$	0.0977
$\text{Hg}_2\text{SO}_4 + 2e \rightleftharpoons 2\text{Hg} + \text{SO}_4^{2-}$	0.613
$\text{I}_2 + 2e \rightleftharpoons 2\text{I}^-$	0.5355
$\text{I}_3^- + 2e \rightleftharpoons 3\text{I}^-$	0.536
$\text{K}^+ + e \rightleftharpoons \text{K}$	-2.925
$\text{Li}^+ + e \rightleftharpoons \text{Li}$	-3.045
$\text{Mg}^{2+} + 2e \rightleftharpoons \text{Mg}$	-2.356
$\text{Mn}^{2+} + 2e \rightleftharpoons \text{Mn}$	-1.18
$\text{Mn}^{3+} + e \rightleftharpoons \text{Mn}^{2+}$	1.5
$\text{MnO}_2 + 4\text{H}^+ + 2e \rightleftharpoons \text{Mn}^{2+} + 2\text{H}_2\text{O}$	1.23
$\text{MnO}_4^- + 8\text{H}^+ + 5e \rightleftharpoons \text{Mn}^{2+} + 4\text{H}_2\text{O}$	1.51
$\text{Na}^+ + e \rightleftharpoons \text{Na}$	-2.714
$\text{Ni}^{2+} + 2e \rightleftharpoons \text{Ni}$	-0.257
$\text{Ni}(\text{OH})_2 + 2e \rightleftharpoons \text{Ni} + 2\text{OH}^-$	-0.72
$\text{O}_2 + 2\text{H}^+ + 2e \rightleftharpoons \text{H}_2\text{O}_2$	0.695
$\text{O}_2 + 4\text{H}^+ + 4e \rightleftharpoons 2\text{H}_2\text{O}$	1.229
$\text{O}_2 + 2\text{H}_2\text{O} + 4e \rightleftharpoons 4\text{OH}^-$	0.401
$\text{O}_3 + 2\text{H}^+ + 2e \rightleftharpoons \text{O}_2 + \text{H}_2\text{O}$	2.075
$\text{Pb}^{2+} + 2e \rightleftharpoons \text{Pb}$	-0.1251
$\text{Pb}^{2+} + 2e \rightleftharpoons \text{Pb}(\text{Hg})$	-0.1205
$\text{PbO}_2 + 4\text{H}^+ + 2e \rightleftharpoons \text{Pb}^{2+} + 2\text{H}_2\text{O}$	1.468
$\text{PbO}_2 + \text{SO}_4^{2-} + 4\text{H}^+ + 2e \rightleftharpoons \text{PbSO}_4 + 2\text{H}_2\text{O}$	1.698
$\text{PbSO}_4 + 2e \rightleftharpoons \text{Pb} + \text{SO}_4^{2-}$	-0.3505
$\text{Pd}^{2+} + 2e \rightleftharpoons \text{Pd}$	0.915
$\text{Pt}^{2+} + 2e \rightleftharpoons \text{Pt}$	1.188
$\text{PtCl}_4^{2-} + 2e \rightleftharpoons \text{Pt} + 4\text{Cl}^-$	0.758
$\text{PtCl}_6^{2-} + 2e \rightleftharpoons \text{PtCl}_4^{2-} + 2\text{Cl}^-$	0.726
$\text{Ru}(\text{NH}_3)_6^{3+} + e \rightleftharpoons \text{Ru}(\text{NH}_3)_6^{2+}$	0.10
$\text{S} + 2e \rightleftharpoons \text{S}^{2-}$	-0.447
$\text{Sn}^{2+} + 2e \rightleftharpoons \text{Sn}$	-0.1375
$\text{Sn}^{4+} + 2e \rightleftharpoons \text{Sn}^{2+}$	0.15
$\text{Tl}^+ + e \rightleftharpoons \text{Tl}$	-0.3363
$\text{Tl}^+ + e \rightleftharpoons \text{Tl}(\text{Hg})$	-0.3338
$\text{Tl}^{3+} + 2e \rightleftharpoons \text{Tl}^+$	1.25
$\text{U}^{3+} + 3e \rightleftharpoons \text{U}$	-1.66
$\text{U}^{4+} + e \rightleftharpoons \text{U}^{3+}$	-0.52
$\text{UO}_2^+ + 4\text{H}^+ + e \rightleftharpoons \text{U}^{4+} + 2\text{H}_2\text{O}$	0.273
$\text{UO}_2^{2+} + e \rightleftharpoons \text{UO}_2^+$	0.163

(continued)

TABLE C.1 (continued)

Reaction	Potential, V
$V^{2+} + 2e \rightleftharpoons V$	-1.13
$V^{3+} + e \rightleftharpoons V^{2+}$	-0.255
$VO^{2+} + 2H^+ + e \rightleftharpoons V^{3+} + H_2O$	0.337
$VO_2^+ + 2H^+ + e \rightleftharpoons VO^{2+} + H_2O$	1.00
$Zn^{2+} + 2e \rightleftharpoons Zn$	-0.7626
$ZnO_2^{2-} + 2H_2O + 2e \rightleftharpoons Zn + 4OH^-$	-1.285

<sup>a</sup> The data in this table are mainly taken from A. J. Bard, J. Jordan, and R. Parsons, Eds., "Standard Potentials in Aqueous Solutions," Marcel Dekker, New York, 1985 (prepared under the auspices of the Electrochemistry and Electroanalytical Chemistry Commissions of IUPAC). Other sources of standard potentials and thermodynamic data include: (1) A. J. Bard and H. Lund, Eds., "The Encyclopedia of the Electrochemistry of the Elements," Marcel Dekker, New York, 1973-1986. (2) G. Milazzo and S. Caroli, "Tables of Standard Electrode Potentials," Wiley-Interscience, New York, 1977. The data here are referred to the NHE based on a 1-atm standard state for H<sub>2</sub>. See the footnote in Section 2.1.5 concerning the recent change in standard state.

Table C.2 Selected Formal Potentials in Aqueous Solution at 25°C in V vs. NHE<sup>a</sup>

Reaction	Conditions	Potential, V
$Cu(II) + e \rightleftharpoons Cu$	1 M NH <sub>3</sub> + 1 M NH <sub>4</sub> <sup>+</sup>	0.01
	1 M KBr	0.52
$Ce(IV) + e \rightleftharpoons Ce(III)$	1 M HNO <sub>3</sub>	1.61
	1 M HCl	1.28
	1 M HClO <sub>4</sub>	1.70
	1 M H <sub>2</sub> SO <sub>4</sub>	1.44
$Fe(III) + e \rightleftharpoons Fe(II)$	1 M HCl	0.70
	10 M HCl	0.53
	1 M HClO <sub>4</sub>	0.735
	1 M H <sub>2</sub> SO <sub>4</sub>	0.68
	2 M H <sub>3</sub> PO <sub>4</sub>	0.46
$Fe(CN)_6^{3-} + e \rightleftharpoons Fe(CN)_6^{4-}$	0.1 M HCl	0.56
	1 M HCl	0.71
	1 M HClO <sub>4</sub>	0.72
$Sn(IV) + 2e \rightleftharpoons Sn(II)$	1 M HCl	0.14

<sup>a</sup> The data in this table are taken mainly from G. Charlot, "Oxidation-Reduction Potentials," Pergamon, London, 1958. Additional values are found in J. J. Lingane, "Electroanalytical Chemistry," Interscience, New York, 1958, and L. Meites, Ed., "Handbook of Analytical Chemistry," McGraw-Hill, New York, 1963.

In class: Cu/Zn demo →

Al/"Cu" demo

↳ What is the rxn that is really happening?

↳ how do we know?

↓  
"Scale-up" to "practical" solution → Aluminium can

↓  
Cu or other rod

→ What happens when we don't have  $\infty$  resistance + current is allowed to flow?

↳ Is this enough energy/power to run anything?

→ Discuss assignment 1 for Battery lab

→ What if our device is not @ STP?  
→  $\Delta G = \Delta G(T, P, N) \dots$

Remember:  $\Delta G = \Delta G(T, P, N)$

↓  
n [e]

How does impact cell voltage?



2 ways to find  $\Delta G(T)$

↓  
1. Method in SUN (attached) →  $\Delta G_p$  method

2. Use [webbook.nist.gov/chemistry](http://webbook.nist.gov/chemistry)  
→ NIST chemistry Webbook

to find  $\Delta G_f(T)$  → Then do  $\Delta G = \text{Products} - \text{Reactants}$

↓  
This is my preferred method,  
but either will work

↓  
Excel spreadsheet attached

↓  
 $\Delta G$  vs T + V vs T

→ Also what is efficiency?

$$\text{TD} = \frac{\Delta G}{\Delta H}$$

$$\text{Voltage eff} = \frac{V}{V_{th}}$$

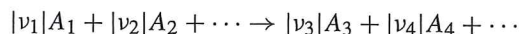
$$\text{total } \gamma = \left(\frac{\Delta G}{\Delta H}\right) \left(\frac{V}{V_{th}}\right)$$

↳ importance? → Later!

## 4.6 TEMPERATURE DEPENDENCE OF $\Delta H^\circ$

In the foregoing sections, standard heats of reaction are discussed for a reference temperature of 298.15 K. In this section we treat the calculation of standard heats of reaction at other temperatures from knowledge of the value at the reference temperature.

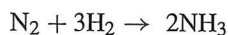
The general chemical reaction may be written:



where  $|\nu_i|$  is a stoichiometric coefficient and  $A_i$  stands for a chemical formula. The species on the left are reactants; those on the right, products. The sign convention for  $\nu_i$  is as follows:

*positive (+) for products and negative (-) for reactants*

The  $\nu_i$  with their accompanying signs are called stoichiometric *numbers*. For example, when the ammonia synthesis reaction is written:



then  $\nu_{\text{N}_2} = -1$      $\nu_{\text{H}_2} = -3$      $\nu_{\text{NH}_3} = 2$

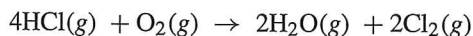
This sign convention allows the definition of a standard heat of reaction to be expressed mathematically by the equation:

$$\Delta H^\circ \equiv \sum_i \nu_i H_i^\circ \quad (4.14)$$

where  $H_i^\circ$  is the enthalpy of species  $i$  in its standard state and the summation is over all products and reactants. The standard-state enthalpy of a chemical compound is equal to its heat of formation plus the standard-state enthalpies of its constituent elements. If the standard-state enthalpies of all elements are arbitrarily set equal to zero as the basis of calculation, then the standard-state enthalpy of each compound is its heat of formation. In this event,  $H_i^\circ = \Delta H_{f_i}^\circ$  and Eq. (4.14) becomes:

$$\Delta H^\circ = \sum_i \nu_i \Delta H_{f_i}^\circ \quad (4.15)$$

where the summation is over all products and reactants. This formalizes the procedure described in the preceding section for calculation of standard heats of other reactions from standard heats of formation. Applied to the reaction,



Eq. (4.15) is written:

$$\Delta H^\circ = 2\Delta H_{f_{\text{H}_2\text{O}}}^\circ - 4\Delta H_{f_{\text{HCl}}}^\circ$$

With data from Table C.4 for 298.15 K, this becomes:

$$\Delta H_{298}^\circ = (2)(-241,818) - (4)(-92,307) = -114,408 \text{ J}$$

in agreement with the result of Ex. 4.5.

For standard reactions, products and reactants are always at the standard-state pressure of 1 bar. Standard-state enthalpies are therefore functions of temperature only, and by Eq. (2.21),

$$dH_i^\circ = C_{P_i}^\circ dT$$

where subscript  $i$  identifies a particular product or reactant. Multiplying by  $\nu_i$  and summing over all products and reactants gives:

$$\sum_i \nu_i dH_i^\circ = \sum_i \nu_i C_{P_i}^\circ dT$$

Since  $\nu_i$  is a constant, it may be placed inside the differential:

$$\sum_i d(\nu_i H_i^\circ) = d \sum_i \nu_i H_i^\circ = \sum_i \nu_i C_{P_i}^\circ dT$$

The term  $\sum_i \nu_i H_i^\circ$  is the standard heat of reaction, defined by Eq. (4.14) as  $\Delta H^\circ$ . The standard heat-capacity change of reaction is defined similarly:

$$\Delta C_P^\circ \equiv \sum_i \nu_i C_{P_i}^\circ \quad (4.16)$$

As a result of these definitions, the preceding equation becomes:

$$d\Delta H^\circ = \Delta C_P^\circ dT \quad (4.17)$$

This is the fundamental equation relating heats of reaction to temperature. Integration gives:

$$\Delta H^\circ = \Delta H_0^\circ + R \int_{T_0}^T \frac{\Delta C_P^\circ}{R} dT \quad (4.18)$$

where  $\Delta H^\circ$  and  $\Delta H_0^\circ$  are heats of reaction at temperature  $T$  and at reference temperature  $T_0$  respectively. If the temperature dependence of the heat capacity of each product and reactant is given by Eq. (4.4), then the integral is given by the analog of Eq. (4.7) ( $\tau \equiv T/T_0$ ):

$$\int_{T_0}^T \frac{\Delta C_P^\circ}{R} dT = (\Delta A)T_0(\tau - 1) + \frac{\Delta B}{2}T_0^2(\tau^2 - 1) + \frac{\Delta C}{3}T_0^3(\tau^3 - 1) + \frac{\Delta D}{T_0} \left( \frac{\tau - 1}{\tau} \right) \quad (4.19)$$

where by definition,

$$\Delta A \equiv \sum_i \nu_i A_i$$

with analogous definitions for  $\Delta B$ ,  $\Delta C$ , and  $\Delta D$ .

An alternative formulation results when a mean heat capacity change of reaction is defined in analogy to Eq. (4.8):

$$\frac{\langle \Delta C_P^\circ \rangle_H}{R} = \Delta A + \frac{\Delta B}{2}T_0(\tau + 1) + \frac{\Delta C}{3}T_0^2(\tau^2 + \tau + 1) + \frac{\Delta D}{\tau T_0^2} \quad (4.20)$$

Equation (4.18) then becomes:

$$\Delta H^\circ = \Delta H_0^\circ + \langle \Delta C_P^\circ \rangle_H (T - T_0) \quad (4.21)$$

### 13.4 EFFECT OF TEMPERATURE ON THE EQUILIBRIUM CONSTANT

Since the standard-state temperature is that of the equilibrium mixture, the standard property changes of reaction, such as  $\Delta G^\circ$  and  $\Delta H^\circ$ , vary with the equilibrium temperature. The dependence of  $\Delta G^\circ$  on  $T$  is given by Eq. (13.13), which may be rewritten:

$$\frac{d(\Delta G^\circ/RT)}{dT} = \frac{-\Delta H^\circ}{RT^2}$$

In view of Eq. (13.11b), this becomes:

$$\boxed{\frac{d \ln K}{dT} = \frac{\Delta H^\circ}{RT^2}} \quad (13.14)$$

Equation (13.14) gives the effect of temperature on the equilibrium constant, and hence on the equilibrium conversion. If  $\Delta H^\circ$  is negative, i.e., if the reaction is exothermic, the equilibrium constant decreases as the temperature increases. Conversely,  $K$  increases with  $T$  for an endothermic reaction.

If  $\Delta H^\circ$ , the standard enthalpy change (heat) of reaction, is assumed independent of  $T$ , integration of Eq. (13.14) from a particular temperature  $T'$  to an arbitrary temperature  $T$  leads to the simple result:

$$\ln \frac{K}{K'} = -\frac{\Delta H^\circ}{R} \left( \frac{1}{T} - \frac{1}{T'} \right) \quad (13.15)$$

This approximate equation implies that a plot of  $\ln K$  vs. the reciprocal of absolute temperature is a straight line. Figure 13.2, a plot of  $\ln K$  vs.  $1/T$  for a number of common reactions, illustrates this near linearity. Thus, Eq. (13.15) provides a reasonably accurate relation for the interpolation and extrapolation of equilibrium-constant data.

The *rigorous* development of the effect of temperature on the equilibrium constant is based on the definition of the Gibbs energy, written for a chemical species in its standard state:

$$G_i^\circ = H_i^\circ - TS_i^\circ$$

Multiplication by  $\nu_i$  and summation over all species gives:

$$\sum_i \nu_i G_i^\circ = \sum_i \nu_i H_i^\circ - T \sum_i \nu_i S_i^\circ$$

As a result of the definition of a standard property change of reaction, this reduces to:

$$\Delta G^\circ = \Delta H^\circ - T \Delta S^\circ \quad (13.16)$$

The standard heat of reaction is related to temperature:

$$\Delta H^\circ = \Delta H_0^\circ + R \int_{T_0}^T \frac{\Delta C_p^\circ}{R} dT \quad (4.18)$$



The temperature dependence of the standard entropy change of reaction is developed similarly. Equation (6.21) is written for the standard-state entropy of species  $i$  at the constant standard-state pressure  $P^\circ$ :

$$dS_i^\circ = C_{P_i}^\circ \frac{dT}{T}$$

Multiplying by  $\nu_i$ , summing over all species, and invoking the definition of a standard property change of reaction yields:

$$d\Delta S^\circ = \Delta C_P^\circ \frac{dT}{T}$$

Integration gives:

$$\Delta S^\circ = \Delta S_0^\circ + R \int_{T_0}^T \frac{\Delta C_P^\circ}{R} \frac{dT}{T} \quad (13.17)$$

where  $\Delta S^\circ$  and  $\Delta S_0^\circ$  are standard entropy changes of reaction at temperature  $T$  and at reference temperature  $T_0$  respectively. Equations (13.16), (4.18), and (13.17) are combined to yield:

$$\Delta G^\circ = \Delta H_0^\circ + R \int_{T_0}^T \frac{\Delta C_P^\circ}{R} dT - T\Delta S_0^\circ - RT \int_{T_0}^T \frac{\Delta C_P^\circ}{R} \frac{dT}{T}$$

However,

$$\Delta S_0^\circ = \frac{\Delta H_0^\circ - \Delta G_0^\circ}{T_0}$$

Whence,

$$\Delta G^\circ = \Delta H_0^\circ - \frac{T}{T_0}(\Delta H_0^\circ - \Delta G_0^\circ) + R \int_{T_0}^T \frac{\Delta C_P^\circ}{R} dT - RT \int_{T_0}^T \frac{\Delta C_P^\circ}{R} \frac{dT}{T}$$

Finally, division by  $RT$  yields:

$$\frac{\Delta G^\circ}{RT} = \frac{\Delta G_0^\circ - \Delta H_0^\circ}{RT_0} + \frac{\Delta H_0^\circ}{RT} + \frac{1}{T} \int_{T_0}^T \frac{\Delta C_P^\circ}{R} dT - \int_{T_0}^T \frac{\Delta C_P^\circ}{R} \frac{dT}{T} \quad (13.18)$$

Recall that by Eq. (13.11b),  $\ln K = -\Delta G^\circ/RT$ .

When the temperature dependence of the heat capacity of each species is given by Eq. (4.4), the first integral on the right side of Eq. (13.18) is given by Eq. (4.19), represented for computational purposes by:

$$\int_{T_0}^T \frac{\Delta C_P^\circ}{R} dT = \text{IDCPH}(T_0, T; DA, DB, DC, DD)$$

where "D" denotes " $\Delta$ ". Similarly, the second integral is given by the analog of Eq. (5.15):

$$\int_{T_0}^T \frac{\Delta C_P^\circ}{R} \frac{dT}{T} = \Delta A \ln \tau + \left[ \Delta B T_0 + \left( \Delta C T_0^2 + \frac{\Delta D}{\tau^2 T_0^2} \right) \left( \frac{\tau + 1}{2} \right) \right] (\tau - 1) \quad (13.19)$$

where

$$\tau \equiv \frac{T}{T_0}$$

Calculating  $\Delta H_{rxn} + \Delta G_{rxn}$  from  
 Shomate Equation  
 ↳ NIST Chemistry Webbook

Species	Hof (kJ/mol)	So (J/mol*K)	A	B	C	D	E
Methane	-74.87	186.25	-0.703029	108.4773	-42.52157	5.862788	0.678565
CO2	-393.52	213.79	24.99735	55.18696	-33.69137	7.948387	-0.136638
Oxygen	0	205.15	31.32234	-20.23531	57.86644	-36.50624	-0.007374
Hydrogen	0	130.68	33.066178	-11.363417	11.432816	-2.772874	-0.158558
Carbon	716.669	158.1	21.1751	-0.812428	0.448537	-0.043256	-0.013103
H2O	-241.83	188.84	30.092	6.832514	6.793435	-2.53448	0.082139
CO	-110.53	197.66	25.56759	6.09613	4.054656	-2.671301	0.131021
Temperature (oc)	Temperature (K)	T(K)/1000	H methane	HO2	H Carbon	H H2O	H CO2
25	298.15	0.29815	-74.87190289	-0.00027175	716.6720711	-241.8258731	-393.5253202
80	353.15	0.35315	-72.85059268	1.62465731	717.8178456	-239.9706621	-391.415172
150	423.15	0.42315	-70.06002527	3.725236139	719.2764554	-237.578723	-388.553384
250	523.15	0.52315	-65.58387918	6.805980067	721.3592218	-234.0836327	-384.1761278
350	623.15	0.62315	-60.51781359	9.98933393	723.4400995	-230.4819825	-379.5140465
425	698.15	0.69815	-56.34486143	12.43883388	724.9994782	-227.7047492	-375.859961
450	723.15	0.72315	-54.88589686	13.26504578	725.5190484	-226.7639611	-374.6154071
475	748.15	0.74815	-53.39406668	14.09514029	726.0385173	-225.8155193	-373.358569
500	773.15	0.77315	-51.87007752	14.92840565	726.5578917	-224.8593599	-372.0899952
525	798.15	0.79815	-50.31464956	15.76404482	727.0771787	-223.8954282	-370.81021
550	823.15	0.82315	-48.72851237	16.60117544	727.5963861	-222.9236785	-369.5197146
575	848.15	0.84815	-47.11240153	17.43882983	728.1155216	-221.9440731	-368.2189876
600	873.15	0.87315	-45.46705579	18.27595491	728.6345934	-220.9565825	-366.9084854
625	898.15	0.89815	-43.79321471	19.1114122	729.1536097	-219.9611848	-365.5886429
650	923.15	0.92315	-42.09161669	19.94397781	729.6725791	-218.9578657	-364.259874
675	948.15	0.94815	-40.36299735	20.77234238	730.19151	-217.9466179	-362.9225715
700	973.15	0.97315	-38.60808804	21.59511111	730.710411	-216.9274415	-361.5771079
725	998.15	0.99815	-36.82761474	22.41080374	731.2292908	-215.9003434	-360.2238352
750	1023.15	1.02315	-35.02229699	23.21785451	731.7481582	-214.8653372	-358.8630854
775	1048.15	1.04815	-33.19284703	24.01461216	732.2670218	-213.8224435	-357.4951705
800	1073.15	1.07315	-31.33996904	24.79933396	732.7858905	-212.7716893	-356.1203829
825	1098.15	1.09815	-29.46435853	25.57021566	733.3047729	-211.7131082	-354.7389952
850	1123.15	1.12315	-27.56670171	26.32533148	733.8236778	-210.6467404	-353.3512605
875	1148.15	1.14815	-25.64767508	27.06269414	734.342614	-209.5726324	-351.9574124
900	1173.15	1.17315	-23.70794495	27.78022483	734.8615899	-208.490837	-350.5576653
925	1198.15	1.19815	-21.74816709	28.47575923	735.3806144	-207.4014137	-349.1522142
950	1223.15	1.22315	-19.76898638	29.14704747	735.899696	-206.3044277	-347.741235
975	1248.15	1.24815	-17.77103657	29.79175415	736.4188432	-205.1999511	-346.3248843
1000	1273.15	1.27315	-15.75493999	30.40745833	736.9380645	-204.0880616	-344.9032999

F	G	H
-76.84376	158.7163	-74.8731
-403.6075	228.2431	-393.5224
-8.903471	246.7945	0
-9.980797	172.707974	0
710.347	183.8734	716.669
-250.881	223.3967	-241.8264
-118.0089	227.3665	-110.5271

$$C_p^\circ = A + B^*t + C^*t^2 + D^*t^3 + E/t^2$$

$$H^\circ - H^\circ_{298.15} = A^*t + B^*t^2/2 + C^*t^3/3 + D^*t^4/4 - E/t + F - H$$

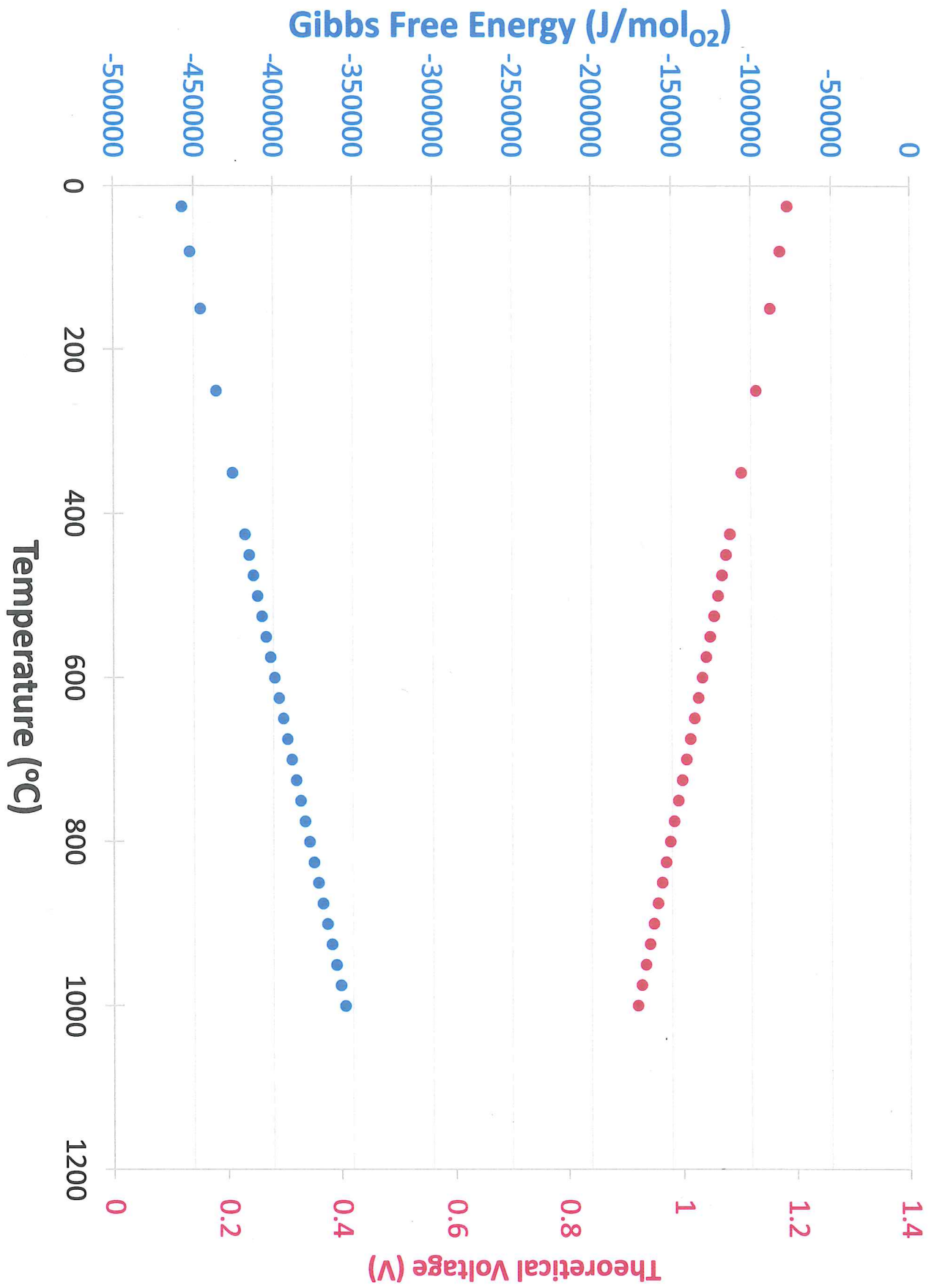
$$S^\circ = A^*\ln(t) + B^*t + C^*t^2/2 + D^*t^3/3 - E/(2^*t^2) + G$$

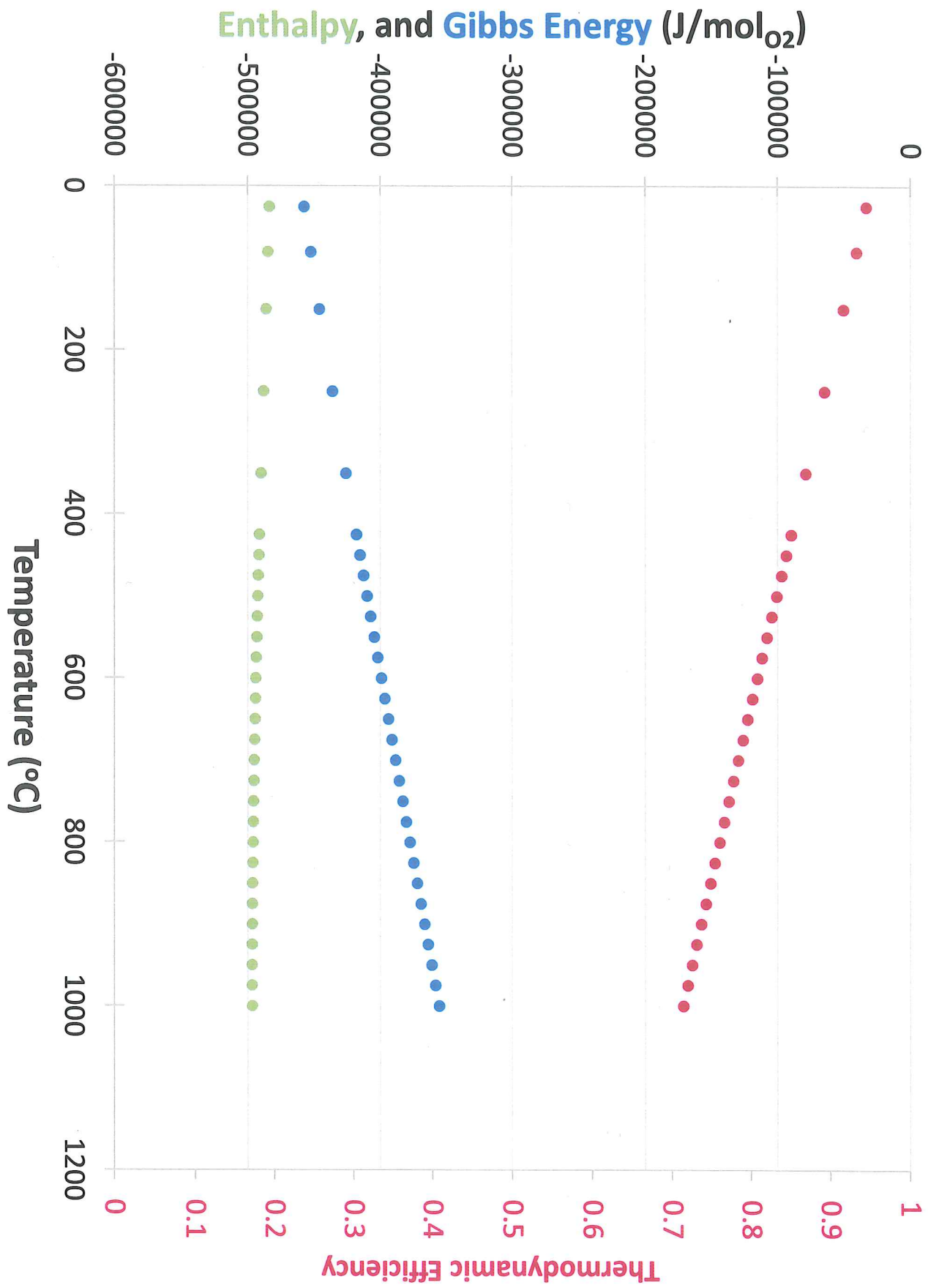
$C_p^\circ$  = heat capacity (J/mol\*K)  
 $H^\circ$  = standard enthalpy (kJ/mol)  
 $S^\circ$  = standard entropy (J/mol\*K)

H CO	H Hydrogen	Smethane	SO2	S carbon	S H2O	S CO2	S CO
-110.5238729	0.000149248	186.2547011	205.1472787	158.0992005	188.8352692	213.7876341	197.6628841
-108.9214338	1.593975211	192.4708852	210.1481735	161.6259924	194.5450771	220.2771571	202.5953443
-106.8728401	3.635041449	199.6694537	215.5730819	165.3940837	200.7227242	227.6630021	207.886893
-103.9059583	6.559574395	209.143036	222.1048394	169.8125579	208.1335244	236.9372443	214.1787761
-100.8767537	9.490177385	217.989701	227.6705444	173.45246	214.4306335	245.0855104	219.4757243
-98.55962807	11.69425212	224.3084721	231.381564	175.8153853	218.6379846	250.6207287	222.9862724
-97.77842269	12.43064372	226.361547	232.5442809	176.5465809	219.9619314	252.3721469	224.0856504
-96.99279547	13.16807305	228.3895245	233.6727583	177.2527852	221.2512828	254.0807381	225.1536723
-96.20276186	13.90665525	230.3931257	234.7683118	177.9356503	222.5083975	255.7485967	226.1923796
-95.40834887	14.64650533	232.3729855	235.8320227	178.5966712	223.7353972	257.377648	227.203604
-94.60959421	15.38773722	234.3296683	236.8647673	179.237205	224.9341965	258.9696676	228.1889946
-93.80654568	16.13046296	236.2636808	237.8672406	179.8584871	226.106528	260.5262992	229.1500403
-92.9992606	16.87479203	238.1754819	238.8399781	180.4616457	227.2539641	262.0490683	230.088089
-92.18780537	17.62083084	240.0654904	239.7833735	181.0477135	228.3779354	263.5393959	231.0043645
-91.37225507	18.36868221	241.9340922	240.697694	181.6176383	229.4797462	264.998609	231.89998
-90.55269315	19.11844504	243.7816451	241.5830942	182.1722921	230.5605887	266.4279506	232.7759506
-89.72921118	19.87021394	245.6084833	242.4396277	182.7124788	231.6215544	267.8285879	233.6332035
-88.90190857	20.62407898	247.4449212	243.2672571	183.2389413	232.6636449	269.2016201	234.4725877
-88.07089243	21.38012543	249.201256	244.0658634	183.7523671	233.6877806	270.5480843	235.2948812
-87.23627735	22.13843358	250.9677708	244.8352534	184.2533943	234.6948085	271.8689622	236.1007988
-86.3981853	22.89907852	252.7147358	245.5751671	184.7426157	235.68551	273.1651844	236.8909974
-85.55674547	23.66213006	254.4424108	246.2852838	185.2205832	236.6606059	274.4376353	237.6660821
-84.71209418	24.42765253	256.1510465	246.9652272	185.6878112	237.6207628	275.6871573	238.4266107
-83.8643748	25.1957047	257.8408854	247.6145706	186.1447803	238.5665976	276.9145543	239.1730978
-83.01373762	25.96633969	259.5121632	248.2328414	186.5919401	239.4986816	278.1205947	239.906019
-82.16033982	26.73960484	261.1651095	248.8195244	187.0297114	240.417545	279.3060148	240.6258138
-81.30434541	27.51554169	262.7999488	249.374066	187.4584893	241.3236797	280.4715209	241.3328889
-80.44592514	28.29418587	264.4169009	249.8958768	187.8786445	242.2175427	281.6177921	242.0276209
-79.58525648	29.07556705	266.0161816	250.3843346	188.2905258	243.0995589	282.7454822	242.7103586

Fuel Cell: 2H2+O2 -> 2H2O

S Hydrogen	Delt H (J/mol)	delt S (J/mol K)	delt G (J/mol)	Vcell	efficiency
130.6801501	-483651.7729	-88.83704046	-457165.0093	1.184545753	0.94523588
135.5855369	-484753.932	-92.22909329	-452183.2277	1.171637617	0.932809819
140.8579734	-486152.765	-95.84358045	-445596.5539	1.154571095	0.916577228
147.0618868	-488092.3942	-99.96156421	-435797.5018	1.129181082	0.892858621
152.1878902	-489933.6537	-103.1850578	-425633.885	1.102846457	0.868758212
155.5276039	-491236.8366	-105.1608026	-417818.8223	1.082597096	0.850544567
156.5639293	-491654.2555	-105.7482767	-415182.3892	1.075765918	0.844460074
157.5664403	-492062.325	-106.3030733	-412531.6807	1.068897751	0.838372823
158.5375116	-492460.4359	-106.8265399	-409867.4965	1.061994668	0.832285127
159.479291	-492847.9119	-107.3198104	-407190.6053	1.05505866	0.826199311
160.3937263	-493224.0069	-107.7838269	-404501.7497	1.048091652	0.820117724
161.282588	-493587.902	-108.2193606	-401801.6513	1.041095512	0.814042746
162.1474894	-493938.704	-108.6270287	-399091.0139	1.034072066	0.807976801
162.9899037	-494275.4436	-109.0073101	-396370.528	1.027023101	0.801922356
163.8111787	-494597.0736	-109.360559	-393640.8736	1.01995038	0.79588193
164.61255	-494902.4684	-109.6870169	-390902.7233	1.012855646	0.7898581
165.3951523	-495190.4221	-109.9868235	-388156.7448	1.005740628	0.783853499
166.1600292	-495459.6485	-110.2600257	-385403.6038	0.998607052	0.777870822
166.9081423	-495708.7798	-110.5065868	-382643.9655	0.99145664	0.771912827
167.6403784	-495936.3663	-110.7263931	-379878.4974	0.984291124	0.765982338
168.357557	-496140.8755	-110.9192612	-377107.8704	0.977112224	0.760082245
169.060436	-496320.6922	-111.084944	-374332.7609	0.969921742	0.754215504
169.7497171	-496474.1173	-111.2231359	-371553.8522	0.9627214	0.748385141
170.426051	-496599.3682	-111.3334774	-368771.8361	0.955513006	0.742594251
171.0900411	-496694.5783	-111.4155602	-365987.4138	0.948298378	0.736846001
171.742248	-496757.7962	-111.4689303	-363201.2974	0.94107936	0.731143628
172.3831928	-496786.9863	-111.4930921	-360414.2107	0.933857828	0.725490443
173.01336	-496780.028	-111.4875114	-357626.8906	0.926635691	0.719889831
173.6332007	-496734.7157	-111.4516184	-354840.0877	0.919414895	0.714345256





What if our reaction is not @ STP?



$$\Delta G = \Delta G^{\circ} + RT \ln \left( \frac{a_R^{\nu_R}}{a_O^{\nu_O}} \right)$$

$$-nFE_{eg} = -nFE^{\circ} + RT \ln \left( \frac{a_R^{\nu_R}}{a_O^{\nu_O}} \right)$$

$$E_{eg} = E^{\circ} - \frac{RT}{nF} \ln \left( \frac{a_R^{\nu_R}}{a_O^{\nu_O}} \right)$$

$$\boxed{E_{eg} = E^{\circ} + \frac{RT}{nF} \ln \left( \frac{a_O^{\nu_O}}{a_R^{\nu_R}} \right)} \Rightarrow \text{Nernst Equation}$$

- for liquid:  $a_i = \gamma_i C_i$
- for vapor:  $a_i = \gamma_i P_i$
- for solid  $a_i \approx 1$

For liquids:

$$E_{eq} = E^{\circ} + \frac{RT}{nF} \ln \left( \frac{\gamma_0^{\nu_0} C_0^{\nu_0}}{\gamma_R^{\nu_R} C_R^{\nu_R}} \right)$$

$$E_{eq} = E^{\circ} + \frac{RT}{nF} \ln \left( \frac{\gamma_0^{\nu_0}}{\gamma_R^{\nu_R}} \right) + \frac{RT}{nF} \ln \left( \frac{C_0^{\nu_0}}{C_R^{\nu_R}} \right)$$

$E^{\circ 1} \equiv$  Formal Potential

$$E^{\circ 1} = E^{\circ} + \frac{RT}{nF} \ln \left( \frac{\gamma_0^{\nu_0}}{\gamma_R^{\nu_R}} \right)$$

When  $\gamma_0 = \gamma_R = 1$ :

$E^{\circ 1} = E^{\circ} \Rightarrow$  Common Assumption!

$$E_{eq} = E^{\circ 1} + \frac{RT}{nF} \ln \left( \frac{C_0^{\nu_0}}{C_R^{\nu_R}} \right)$$



Most Common Form of the Nernst Eqn!

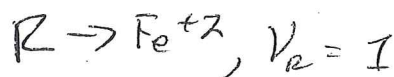
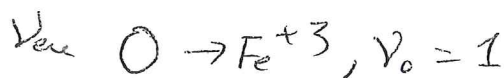
$\rightarrow$  relate to Al/Air cell

$[O_2] \sim 2 \times 10^{-4} M$

$[Al^{3+}] \sim$  very low (initially  $\sim 0$ !)



Example 1:



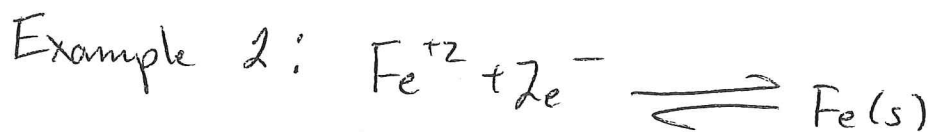
•

$$E_{\text{eq}} = E^{01} + \frac{RT}{nF} \ln \frac{[\text{Fe}^{+3}]}{[\text{Fe}^{+2}]}$$

if we assume:  $\gamma_{\text{O}} = \gamma_{\text{R}} \approx 1$   
 $E^{01} \approx E^0$

$$E_{\text{eq}} = E^0 + \frac{RT}{nF} \ln \frac{[\text{Fe}^{+3}]}{[\text{Fe}^{+2}]}$$

$$E_{\text{eq}} = 0.77 \text{V} + \frac{RT}{nF} \ln \frac{[\text{Fe}^{+3}]}{[\text{Fe}^{+2}]}$$



Assume  $\gamma_{\text{Fe}(s)} = 1$

$$E_{\text{eq}} = \cancel{E^0} E^0 + \frac{RT}{nF} \ln \left( \frac{a_{\text{Fe}^{+2}}}{a_{\text{Fe}}} \right)$$

$$E_{\text{eq}} = E^0 + \frac{RT}{nF} \ln a_{\text{Fe}^{+2}} = E^0 + \frac{RT}{nF} \ln (\gamma_{\text{Fe}^{+2}} C_{\text{Fe}^{+2}})$$

$$E_{\text{eq}} = E^0 + \frac{RT}{nF} \ln [\text{Fe}^{+2}]$$

$$E_{\text{eq}} = -0.44 + \frac{RT}{nF} \ln [\text{Fe}^{+2}]$$